

Advanced Scaling Techniques for the Modeling of Materials Processing

John A. Roubidoux, Patricio F. Mendez, Colorado School of Mines, Center for Welding Joining and Coatings Research

Grant Number: DMI-0547649 NSF Program: Materials Processing and Manufacturing

OMS Methodology Flow Sheet:

Determine the governing equation and boundary conditions that represent the physical process

Normalize the variables and boundary conditions and scale the governing equation.

Determine the vector of inputs and outputs. Build the Matrix of Balances.

Construct Matrix of Coefficients from the coefficients of each term of the scaled governing equation. Obtain the Normalized Matrix of Coefficients.

Perform matrix operation to obtain the Matrix of Estimations. Results in a scaling equation that captures the dominant driving forces involved in the process. The scaling equation is an estimate of unknown process variables.

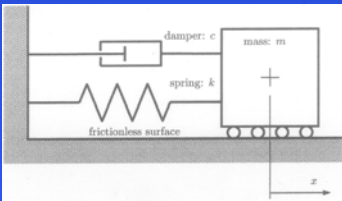
Check for Self-Consistency.

Order of Magnitude Scaling (OMS)

OMS deals with a system of coupled differential equations in their full complexity and provides an approximate solution to the set of governing equations. The solution is expressed in the form of power-laws, and it discriminates the dominant forces in the problem from the less relevant ones. OMS is an improvement over classical scaling techniques due to a more accurate scaling of the differential expressions. OMS lends itself to being implemented in a computer algorithm since the operations potentially involve a large number of matrices that could have a significant number of elements.

Example: Using OMS to obtain an expression for the unknown characteristic time, t_c . (Mechanical Oscillator)

OMS takes advantage of the following feature of governing equations in engineering problems: Each equation is a sum of terms, with each term representing a driving force. The competing driving forces in the Mechanical Oscillator example are: 1). Inertial force 2). Damping force 3). Spring force

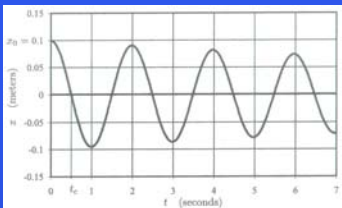


Governing Equation:

$$m\ddot{x} + c\dot{x} + kx = 0 \quad x(0) = 0 \quad \dot{x}(0) = 0$$

Normalizing the variables:

$$x^* = \frac{x - x_{\min}}{x_{\max} - x_{\min}} = \frac{x - 0}{x_0 - 0} = \frac{x}{x_0} \quad \therefore x = x^* x_0 \quad t^* = \frac{t - t_{\min}}{t_{\max} - t_{\min}} = \frac{t - 0}{t_c - 0} = \frac{t}{t_c} \quad \therefore t = t^* t_c$$



Scaled Governing Equation:

$$2 \frac{m x_0}{t_c^2} f_1^*(t^*) + 2 \frac{c x_0}{t_c} f_2^*(t^*) + k x_0 f_3^*(t^*) = 0$$

Vector of Inputs and Outputs:

$$\{\phi\} = \{-1 \quad -1 \quad 1\}$$

The Matrix of Balances:

$$[B] = [1 \quad 1 \quad 3] \quad \text{and} \quad [B]_1 = [1 \quad 2 \quad 3]$$

Matrix of Coefficients (MOC):

$$[C] = \begin{bmatrix} 2 & m & c & k & x_0 & t_c \\ 1 & 1 & 0 & 0 & 1 & -2 \\ 1 & 0 & 1 & 0 & 1 & -1 \\ 0 & 0 & 0 & 1 & 1 & 0 \end{bmatrix}$$

Matrix of Normalized Coefficients: Balance $[B]_1$

$$[N] = \begin{bmatrix} 2 & m & c & k & x_0 & t_c \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & -1 & 1 & 0 & 0 & 1 \\ -1 & -1 & 0 & 1 & 0 & 2 \end{bmatrix}$$

Matrix of Estimations (MOE):

$$[S] = -[N_o]_1^T [N_o]_p = -\left[\frac{1}{2}\right] [-1 \quad -1 \quad 0 \quad 1 \quad 0] = \left[\frac{1}{2} \quad \frac{1}{2} \quad 0 \quad -\frac{1}{2} \quad 0\right]$$

This leads to an estimation of the characteristic time: $\hat{t}_c = \sqrt{\frac{2m}{k}}$

Modeling Friction Stir Welding (FSW) with OMS

➤ The Welding Institute invented Friction Stir Welding in 1991

➤ Solid State Process that joins metal through mechanical deformation

➤ Can weld previously reported unweldable Al alloys (2xxx, 7xxx)

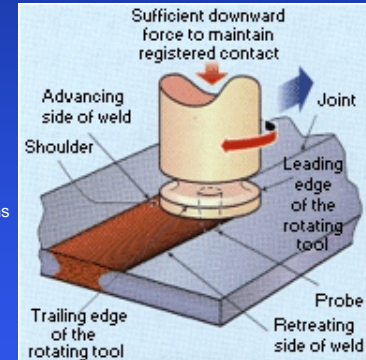
➤ Weld strength is 30-50% greater than with arc welding.

Objective of Research:

- Scale steady state FSW process parameters in high melting temperature alloys.
- No known scaling laws for FSW
- Test with Aluminum
- Scale up to high temperature melting alloys

Analysis:

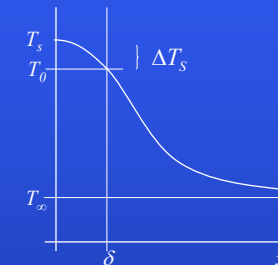
- Five coupled differential equations
- Shear Layer
 - I. Heat Transfer (1)
- I. Deformation (2)
 - I. Constitutive Law (1)
- Base Plate
 - I. Heat Transfer (1)



Governing Equation:

$$\frac{\partial^2 T}{\partial x^2} + \frac{q}{k} = 0 \quad T'(0) = 0, \quad T(\delta) = T_0$$

Heat Transfer in Shear Layer:



Normalizing the variables:

$$x^* = \frac{x - x_{\min}}{x_{\max} - x_{\min}} = \frac{x - 0}{\delta - 0} = \frac{x}{\delta} \quad \therefore x = x^* \delta$$

$$T^* = \frac{T - T_{\min}}{T_{\max} - T_{\min}} = \frac{T - T_0}{\Delta T_s} \quad \therefore T = T_0 + \Delta T_s T^*$$

$$q^* = \frac{q - q_{\min}}{q_{\max} - q_{\min}} = \frac{q - 0}{q_c - 0} = \frac{q}{q_c} \quad \therefore q = q^* q_c$$

Scaled Governing Equation:

$$\frac{2 \Delta T_s k}{\delta^2 q_c} \left(\frac{\partial^2 T}{\partial x^2} \right)^* + q^* = 0$$

OM(1) OM(1)

Scaling Equations:

Heat Transfer in Shear Layer:

$$2 \frac{\Delta T_s k}{\delta^2 \hat{q}_c} = 1$$

Estimate of Shear Layer thickness:

$$\frac{\delta}{a} = \left[2 \left(\frac{\tau_1 \Delta T_m^{1/2} \omega^{1/2} f^{1/2}}{k v_1^{1/2} \Delta T_0^{1+1/2}} \right) (a^2 \omega f) \right]^{1/2}$$

material properties process parameters

The estimation of the shear layer thickness is only obtained by scaling the complete system of equations mentioned in the Analysis section above.

Conclusion:

Order of Magnitude Scaling (OMS) is a modeling technique that deals with a system of coupled differential equations in their full complexity. The solution of the system is expressed in the form of power-laws. The advantage of OMS over other modeling techniques is a resultant scaling equation that is based on system process parameters.