

ASSIGNMENT 1: SOLUTIONS

1a) USE $PV = nRT$

$$\Rightarrow n = PV/(RT)$$
$$\approx (1.5 \times 10^6 \text{ Pa})(0.5 \text{ m}^3) / [(8.315 \frac{\text{J}}{\text{mol} \cdot \text{K}})(293.15 \text{ K})]$$

$\leftarrow 273.15 + 20$

$$\Rightarrow \boxed{n \approx 308 \text{ mol}}$$

b) FOR O_2 THE MASS/MOL IS $2 \times (15.9994 \text{ g/mol}) = 31.999 \text{ g/mol}$

THE MASS OF 308 MOL IS

$$m = (308 \text{ mol})(31.999 \text{ g/mol})(1 \text{ kg}/1000 \text{ g})$$
$$\Rightarrow \boxed{m \approx 9.86 \text{ kg}}$$

c) THE # MOLES AND VOLUME IS UNCHANGED AFTER HEATING,

$$\Rightarrow P = nRT/V$$
$$\approx (308 \text{ mol})(8.315 \frac{\text{J}}{\text{mol} \cdot \text{K}})(773.15 \text{ K})(0.5 \text{ m}^3)$$

$\leftarrow 273.15 + 500$

$$\Rightarrow \boxed{P \approx 3.96 \times 10^6 \text{ Pa}}$$

d) AFTER REMOVAL THE FINAL PRESSURE IS

$$P' = 0.9 P_0 (\approx 1.35 \times 10^6 \text{ Pa})$$

THE TEMPERATURE AND VOLUME ARE FIXED. SO FINAL # MOLES IS

$$n' = P'V/(RT)$$
$$= (0.9 P_0)V/(RT) = 0.9 (P_0 V/(RT)) = 0.9 n (\approx 277 \text{ mol})$$

SO FINAL MASS IS

$$m' = 0.9 m (\approx 8.87 \text{ kg})$$

THE MASS REMOVED IS $m - m' = 0.1 m = \boxed{0.986 \text{ kg}}$

2) AT THE CRITICAL POINT $\frac{dP}{dV} = 0$ AND $\frac{d^2P}{dV^2} = 0$ ON ISOTHERM $T = T_c$.
 HERE THE CRITICAL VOLUME, TEMPERATURE AND PRESSURE ARE V_c, T_c AND P_c .

$$0 = \left. \frac{dP}{dV} \right|_{V_c} = \left[-\frac{RT}{(V-b)^2} e^{-\frac{a}{RTV}} + \frac{RT}{V-b} \frac{a}{RTV^2} e^{-\frac{a}{RTV}} \right] \Big|_{V=V_c}$$

THIS SIMPLIFIES TO GIVE

$$0 = \left[-1 + (V-b) \frac{a}{RT_c V^2} \right] \Big|_{V=V_c}$$

$$\Rightarrow V_c - b = \frac{RT_c}{a} V_c^2 \quad (*)$$

$$0 = \left. \frac{d^2P}{dV^2} \right|_{V_c} = \left[2 \frac{RT_c}{(V-b)^3} e^{-\frac{a}{RT_c V}} - \frac{RT_c}{(V-b)^2} \frac{a}{RT_c V^2} e^{-\frac{a}{RT_c V}} - \frac{RT_c}{(V-b)^2} \frac{a}{RT_c V} e^{-\frac{a}{RT_c V}} + \frac{RT_c}{(V-b)} \left(-2 \frac{a}{RT_c V^3} \right) e^{-\frac{a}{RT_c V}} + \frac{RT_c}{(V-b)} \left(\frac{a}{RT_c V^2} \right)^2 e^{-\frac{a}{RT_c V}} \right] \Big|_{V=V_c}$$

CAN SIMPLIFY BY CANCELLING EXPONENTIALS.

ALSO USE (*) TO REPLACE ALL OCCURRENCES OF $V_c - b$ WITH $\frac{RT_c}{a} V_c^2$

$$\Rightarrow 0 = 2 \frac{a^3}{(RT_c)^2} \frac{1}{V_c^6} - \frac{a^2}{RT_c} \frac{1}{V_c^4} \left(\frac{a}{RT_c V_c^2} \right) - \frac{a^2}{RT_c} \frac{1}{V_c^4} \left(\frac{a}{RT_c V_c} \right) + a \frac{1}{V_c^2} \left(-2 \frac{a}{RT_c V_c^3} \right) + a \frac{1}{V_c^2} \left(\frac{a}{RT_c V_c^2} \right)^2$$

$$\times \frac{(RT_c)^2}{a^3} V_c^6$$

$$\Rightarrow 0 = 2 - 1 - 1 - 2 \frac{RT_c}{a} V_c + 1 = -2 \frac{RT_c}{a} V_c + 1$$

$$\Rightarrow \frac{RT_c}{a} = \frac{1}{2V_c}$$

PUT THIS IN (*) $\Rightarrow V_c - b = \left(\frac{1}{2V_c} \right) V_c^2 = \frac{1}{2} V_c$

$$\Rightarrow \boxed{V_c = 2b}$$

$$\begin{aligned}
 30) \rho &= \rho_0 [1 - \alpha_T(T - T_0) + \alpha_S(S - S_0)] \\
 &\approx \rho_0 [1 - (2.1 \times 10^{-4} \text{ K}^{-1})(25 - 20) \text{ K} + (6.7 \times 10^{-4} \text{ ppt}^{-1})(35 - 38.5 \text{ ppt})] \\
 &\quad \uparrow (\text{DIFFERENCE IN } ^\circ\text{C EQUALS DIFFERENCE IN K}) \\
 &\approx \rho_0 [1 - 1.05 \times 10^{-3} - 2.345 \times 10^{-3}] \\
 &\approx \rho_0 0.9966 \quad \text{WITH } \rho_0 = 1025 \text{ kg/m}^3 \\
 &\approx \boxed{1021.5 \text{ kg/m}^3}
 \end{aligned}$$

b) THE INITIAL VOLUME IN THE BOX IS $V_0 = h_0 A$.
 IF THE INITIAL DENSITY IS ρ_0 , THE MASS IS $M_0 = \rho_0 V_0 = \rho_0 h_0 A$.

IF THE TEMPERATURE CHANGES, THE MASS IS THE SAME. BUT THE DENSITY CHANGES TO $\rho = \rho_0 [1 - \alpha_T \Delta T]$. *

SO THE NEW VOLUME IS $V = M_0 / \rho = \frac{1}{\rho} (\rho_0 h_0 A)$

BECAUSE THE AREA IS THE SAME, THE NEW HEIGHT IS

$$\begin{aligned}
 h &= \frac{V}{A} = \frac{1}{\rho} \rho_0 h_0 \\
 \text{USE (*) } \Rightarrow h &= \frac{1}{\rho_0 (1 - \alpha_T \Delta T)} \rho_0 h_0 = \frac{1}{1 - \alpha_T \Delta T} h_0
 \end{aligned}$$

THE INCREASE IN DEPTH IS $\Delta h = h - h_0 = \left(\frac{1}{1 - \alpha_T \Delta T} - 1 \right) h_0$.

NOW, IF $|\alpha_T \Delta T| \ll 1$, WE CAN APPROXIMATE $\frac{1}{1 - \alpha_T \Delta T} \approx 1 + \alpha_T \Delta T$

$$\Rightarrow \Delta h \approx (1 + \alpha_T \Delta T - 1) h_0 = \boxed{\alpha_T \Delta T h_0}$$

c) WHEN THE TOP km OF SEA WATER WARMS, IT CAN ONLY EXPAND VERTICALLY, NOT Laterally (CONSTRAINED BY CONTINENTS)

SO THIS IS LIKE OUR WATER IN A BOX WITH $\Delta T = 1^\circ\text{C} = 1\text{K}$, $h_0 = 1\text{km}$

$$\Delta h \approx (2.1 \times 10^{-4} \text{ K}^{-1})(1\text{K})(1000\text{m})$$

$$= 0.21 \text{ m}$$

$$\Rightarrow \boxed{\Delta h = 20 \text{ cm}}$$

4) BY DEFINITION, EXPANSIVITY IS

$$\beta \equiv \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_P = \frac{1}{v} \left(\frac{\partial v}{\partial T} \right)_P, \text{ WHERE } V \text{ IS VOLUME AND } v = \frac{V}{M} = \frac{1}{\rho} \text{ SPECIFIC VOLUME}$$

ISOTHERMAL COMPRESSIBILITY IS

$$\kappa \equiv -\frac{1}{V} \left(\frac{\partial V}{\partial P} \right)_T = -\frac{1}{v} \left(\frac{\partial v}{\partial P} \right)_T$$

IN WHICH WE ASSUME $v = v(T, P)$

$$\text{GIVEN } \beta = b \frac{T}{v} \Rightarrow \frac{1}{v} \left(\frac{\partial v}{\partial T} \right)_P = b \frac{T}{v}$$

$$\Rightarrow \left(\frac{\partial v}{\partial T} \right)_P = bT$$

$$\Rightarrow v = \frac{1}{2} b T^2 + f(P) \quad \leftarrow \text{SOME FUNCTION OF PRESSURE} \quad (*)$$

$$\text{GIVEN } \kappa = a \frac{1}{v} \Rightarrow -\frac{1}{v} \left(\frac{\partial v}{\partial P} \right)_T = a \frac{1}{v}$$

$$\Rightarrow \left(\frac{\partial v}{\partial P} \right)_T = -a$$

$$\text{USE } (*) \Rightarrow \left(\frac{\partial}{\partial P} \left(\frac{1}{2} b T^2 + f(P) \right) \right)_T = -a$$

$$\Rightarrow f'(P) = -a$$

$$\Rightarrow f(P) = -aP + C \quad \leftarrow \text{CONSTANT}$$

$$\text{PUT IN } (*) \Rightarrow v = \frac{1}{2} b T^2 - aP + C$$

$$\Rightarrow \boxed{v - \frac{1}{2} b T^2 + aP = C}$$