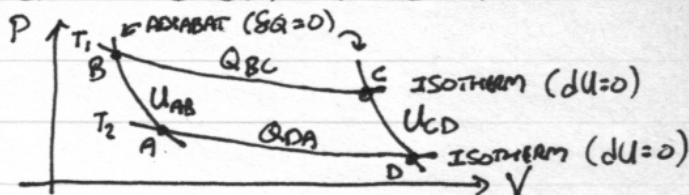


# ⑥ THE SECOND LAW OF THERMODYNAMICS

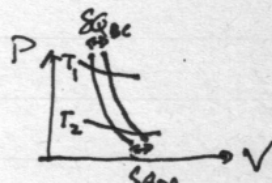
## 1] THERMODYNAMIC DEFINITION OF ENTROPY

RECALL OUR CONSIDERATION OF ENERGY AT EACH STEP IN THE CARNOT HEAT ENGINE



CONSISTENT WITH  $dU = 0$  ALONG ISOTHERMS FOUND  $U_{CD} = -U_{AB}$   
ALONG  $\overline{BC}$  AND  $\overline{DA}$  FOUND THAT HEATS WERE RELATED BY  
$$\frac{1}{T_2} Q_{DA} = - \frac{1}{T_1} Q_{BC} \quad (*)$$

WE ARRIVED AT THIS EXPRESSION ALL THE HEAT WENT IN AND CAME OUT OF  $PdV$  WORK. I.E. NO ADDITIONAL LOSSES DUE TO RADIATION, HEAT DIFFUSION, etc. I.E. A REVERSIBLE PROCESS.



NOW SUPPOSE THE HEATS IN AND OUT ARE VERY SMALL

SO WE CAN WRITE  $Q_{DA} \rightarrow \delta Q_{DA}$ ,  $Q_{BC} \rightarrow \delta Q_{BC}$  AS INFINITESIMALS

THE RESULT (\*) INSPIRES US TO DEFINE A DIFFERENTIAL

$$\boxed{dS \equiv \frac{1}{T} \delta Q}$$

THIS IS THE CLAPEYRON DEFINITION OF ENTROPY,  $S$ . (1843)  
[IT WORKS FOR ALL SUBSTANCES, NOT JUST AN IDEAL GAS]

NOTE, IN GOING AROUND THE CARNOT CYCLE

$$\begin{aligned} \oint dS &= \int_A^B \frac{1}{T} \delta Q + \int_B^C \frac{1}{T_1} \delta Q + \int_C^D \frac{1}{T} \delta Q + \int_D^A \frac{1}{T_2} \delta Q \\ &= 0 + \frac{1}{T_1} Q_{BC} + 0 + \frac{1}{T_2} Q_{DA} \\ &= 0 \quad (\text{USING } (*)) \end{aligned}$$

SO, IN A REVERSIBLE PROCESS  $\oint dS = 0$

$\Rightarrow S$  IS INDEPENDENT OF PATH

$\Rightarrow S$  IS A STATE VARIABLE, LIKE  $U, P, T, V$  etc

## 2] THE SECOND LAW OF THERMODYNAMICS

IN IRREVERSIBLE PROCESSES SOME ENERGY FROM WORK (e.g.  $PdV$ ) IS LOST (e.g. THROUGH FRICTION) BEING TRANSFORMED INTO RADIATED OR CONDUCTED HEAT ENERGY THAT CAN NEVER BE RETURNED AS WORK. [LIKEWISE, A BATTERY CAN PASS A CURRENT THROUGH A RESISTOR HEATING IT UP, BUT HEATING A RESISTOR WILL NOT CHARGE A BATTERY].

So we can write

$$\underbrace{\delta W}_{\text{TOTAL WORK OF SYSTEM ON ENVIRONMENT}} = \underbrace{\delta W_r}_{\text{REVERSIBLE WORK (e.g. } PdV)} + \underbrace{E}_{\text{DISSIPATIVE WORK}}, \quad E > 0$$

BY ENERGY CONSERVATION, THE DISSIPATIVE WORK BECOMES HEAT WHICH IS NOT PART OF A REVERSIBLE PROCESS

So we can write

$$\underbrace{\delta Q}_{\text{TOTAL HEAT of SYSTEM}} = \underbrace{\delta Q_r}_{\text{HEAT FROM REVERSIBLE WORK}} - \underbrace{E}_{\text{HEAT LOST BY DISSIPATION}}$$

NOTE, THE INTERNAL ENERGY DOESN'T CHANGE WHETHER REVERSIBLE OR NOT

$$dU = \delta Q - \delta W = (\delta Q_r - E) - (\delta W_r - E) = \delta Q_r - \delta W_r$$

IMPORTANTLY,  $E > 0$  so  $\delta Q_r \geq \delta Q$  WITH EQUALITY ONLY FOR REVERSIBLE PROCESSES.

RECASTING THIS IN TERMS OF ENTROPY, WHICH NOW IS DEFINED EXPLICITLY FOR HEAT ASSOCIATED WITH REVERSIBLE PROCESSES:

$$\Rightarrow dS = \frac{\delta Q_r}{T} \geq \frac{\delta Q}{T} \geq 0$$

So  $dS \geq 0$  WITH EQUALITY FOR ADIABATIC PROCESSES ( $\delta Q = 0$ )

THIS IS 2<sup>ND</sup> LAW OF THERMODYNAMICS: ENTROPY ALWAYS INCREASES OR, AT BEST, IS CONSTANT.

### 3] FIRST LAW OF THERMODYNAMICS (REPRISE)

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BEFORE WE HAD  $du = \delta Q - p dv$

NOW, WITH  $\delta S \equiv \frac{\delta Q}{T}$  WE CAN WRITE THE 1<sup>ST</sup> LAW IN TERMS OF DIFFERENTIALS IN EACH TERM:

$$\boxed{du = T ds - p dv}$$

THUS WE THINK OF  $U \equiv U(S, V)$ , AND IT IS UNDERSTOOD THAT  $T = T(S, V)$ ,  $P(S, V)$  IN GENERAL.

COMPARE WITH TOTAL DIFFERENTIAL OF  $U$ :  $du = \left(\frac{\partial u}{\partial S}\right)_v ds + \left(\frac{\partial u}{\partial V}\right)_s dv$

SO (AT LAST) WE HAVE AN EXPLICIT (THOUGH NOT INTUITIVE) DEFINITION OF TEMPERATURE:

$$T = \left(\frac{\partial u}{\partial S}\right)_v$$

ALSO

$$P = -\left(\frac{\partial u}{\partial V}\right)_s$$

ALTERNATELY, WE CAN WRITE 1<sup>ST</sup> LAW IN TERMS OF ENTHALPY:

$$\boxed{dH = T ds + V dp}$$

IN WHICH WE UNDERSTAND  $H \equiv H(S, P)$

AGAIN COMPARED WITH  $dH = \left(\frac{\partial H}{\partial S}\right)_p ds + \left(\frac{\partial H}{\partial P}\right)_s dp$

$$\Rightarrow T = \left(\frac{\partial H}{\partial S}\right)_p ; V = \left(\frac{\partial H}{\partial P}\right)_s$$

THESE FORMULAE CAN ALSO BE WRITTEN IN INTRINSIC PROPERTIES

$$du = T ds - p dv$$

$$dh = T ds + v dp$$

$s = \frac{1}{n} S$  (OR  $\frac{1}{M} S$ ) IS THE "SPECIFIC ENTROPY"

## 4] GIBBS + HELMHOLTZ FREE ENERGIES

$U^{(S,V)}$  (INTERNAL ENERGY) AND  $H^{(S,P)}$  (ENTHALPY) ARE TWO OF FOUR COMMONLY USED ENERGIES IN THERMODYNAMICS. THE OTHER TWO REPLACE  $S$  WITH  $T$  AS THE STATE VARIABLE.

HELMHOLTZ FREE ENERGY:  $F \equiv U - TS$ ,  $F = F(T, V)$   
 $\Rightarrow dF = dU - TdS - SdT \stackrel{\text{1st law}}{=} \underline{-SdT - PdV}$

GIBBS FREE ENERGY:  $G \equiv U - TS + PV = H - TS$ ,  $G = G(T, P)$   
 $\Rightarrow \boxed{dG = -SdT + VdP}$

WE WILL SEE THAT GIBBS FREE ENERGY IS PARTICULARLY USEFUL TO STUDY PHASE TRANSFORMATIONS (FOR WHICH  $T$  AND  $P$  ARE CONSTANTS).

THE GIBBS FREE ENERGY IS ALSO USED (AS OF 2010) TO CHARACTERIZE THE THERMODYNAMIC PROPERTIES OF SEA WATER. THIS IS BECAUSE THE ARGUMENTS TO  $G$  ARE DIRECTLY MEASURABLE.

THE FOUR QUANTITIES  $U$ ,  $H$ ,  $F$  AND  $G$  ARE CALLED  
"THERMODYNAMIC POTENTIALS"

THE EXPRESSIONS OF THE 1<sup>ST</sup> LAW FOR  $dU$ ,  $dH$ ,  $dF$ ,  $dG$  ARE CALLED "THERMODYNAMIC IDENTITIES"

## 5] MAXWELL RELATIONS

WE FOUND  $dU = TdS - PdV \Rightarrow T = \left(\frac{\partial U}{\partial S}\right), P = -\left(\frac{\partial U}{\partial V}\right)$

ASSUMING  $U(S, V)$  IS "NICE" (AKA TWICE DIFFERENTIABLE etc)  
 WE KNOW  $\frac{\partial^2 U}{\partial S \partial V} = \frac{\partial^2 U}{\partial V \partial S}$  (ORDER OF DERIVATIVES DOESN'T MATTER)

AND SO WE HAVE  $\boxed{\left(\frac{\partial T}{\partial V}\right)_S = -\left(\frac{\partial P}{\partial S}\right)_V}$

THIS IS ONE OF MAXWELL'S RELATIONS. ANOTHER RELATION  
 IS FOUND FROM ENTHALPY:

$$dH = TdS + VdP \Rightarrow T = \left(\frac{\partial H}{\partial S}\right)_P, V = \left(\frac{\partial H}{\partial P}\right)_S$$

$$\Rightarrow \boxed{\left(\frac{\partial T}{\partial P}\right)_S = \left(\frac{\partial V}{\partial S}\right)_P}$$

FROM HELMHOLTZ FREE ENERGY:

$$dF = -SdT - PdV \Rightarrow S = -\left(\frac{\partial F}{\partial T}\right)_V, P = -\left(\frac{\partial F}{\partial V}\right)_T$$

$$\Rightarrow \boxed{\left(\frac{\partial S}{\partial V}\right)_T = \left(\frac{\partial P}{\partial T}\right)_V}$$

FROM GIBBS FREE ENERGY:

$$dG = -SdT + VdP \Rightarrow S = -\left(\frac{\partial G}{\partial T}\right)_P, V = \left(\frac{\partial G}{\partial P}\right)_T$$

$$\Rightarrow \boxed{\left(\frac{\partial S}{\partial P}\right)_T = -\left(\frac{\partial V}{\partial T}\right)_P}$$

## 6] RECIPROCAL RELATIONS + CYCLICAL RELATIONS

IN WHAT FOLLOWS WE WILL NEED SOME USEFUL IDENTITIES INVOLVING 3 PROPERTIES  $x, y, z$  (e.g.  $P, V, T$ ) INTERRELATED BY SOME FORMULA EXPRESSED ABSTRACTLY AS  $f(x, y, z) = 0$ .

WRITTEN EXPLICITLY AS  $x = x(y, z)$ , WE GET THE DIFFERENTIAL

$$dx = \left(\frac{\partial x}{\partial y}\right)_z dy + \left(\frac{\partial x}{\partial z}\right)_y dz \quad (1)$$

WRITTEN EXPLICITLY AS  $y = y(x, z)$ , WE GET THE DIFFERENTIAL

$$dy = \left(\frac{\partial y}{\partial x}\right)_z dx + \left(\frac{\partial y}{\partial z}\right)_x dz \quad (2)$$

SUBSTITUTING (2) INTO (1) GIVES

$$dx = \left(\frac{\partial x}{\partial y}\right)_z \left(\frac{\partial y}{\partial x}\right)_z dx + \left[ \left(\frac{\partial x}{\partial y}\right)_z \left(\frac{\partial y}{\partial z}\right)_x + \left(\frac{\partial x}{\partial z}\right)_y \right] dz \quad (3)$$

IF  $x$  &  $z$  ARE CONSIDERED AS THE INDEPENDENT VARIABLES, THEN

(3) HOLDS FOR ALL  $dx$  &  $dz$ .

IN PARTICULAR, IF  $dz = 0$  AND  $dx \neq 0$ , (3)  $\Rightarrow \left(\frac{\partial x}{\partial y}\right)_z \left(\frac{\partial y}{\partial x}\right)_z = 1$

$$\Rightarrow \boxed{\left(\frac{\partial x}{\partial y}\right)_z = \frac{1}{\left(\frac{\partial y}{\partial x}\right)_z}} \quad \text{THE "RECIPROCAL RELATION"} \quad (4)$$

IF  $dx = 0$  AND  $dz \neq 0$ , (3)  $\Rightarrow \left(\frac{\partial x}{\partial y}\right)_z \left(\frac{\partial y}{\partial z}\right)_x = - \left(\frac{\partial x}{\partial z}\right)_y \quad (5)$

SOMETIMES (5) IS REWRITTEN USING THE RECIPROCAL RELATION  $\left(\frac{\partial x}{\partial z}\right)_y = \frac{1}{\left(\frac{\partial z}{\partial x}\right)_y}$

$$\Rightarrow \boxed{\left(\frac{\partial x}{\partial y}\right)_z \left(\frac{\partial y}{\partial z}\right)_x \left(\frac{\partial z}{\partial x}\right)_y = -1} \quad \text{THE "CYCLICAL RELATION"} \quad (6)$$

THE NEGATIVE SIGN IS A RESULT OF CHANGING SUBSCRIPTS IN (6).

DO NOT CONFUSE (5) WITH THE CHAIN RULE OF DIFFERENTIATION:

$$\left(\frac{\partial x}{\partial z}\right)_u = \left(\frac{\partial x}{\partial y}\right)_u \left(\frac{\partial y}{\partial z}\right)_u \quad \leftarrow \text{NO NEGATIVE SIGN}$$

IN WHICH  $u \equiv u(x, y)$  FIXED IMPLICITLY RELATES  $x$  &  $y$